

Soft Switching



← Hard Switching
se $i \text{ e } v$ sono $\neq 0$
durante la commutazione

PERDITA PER SWITCHING
(COMMUTAZIONE)

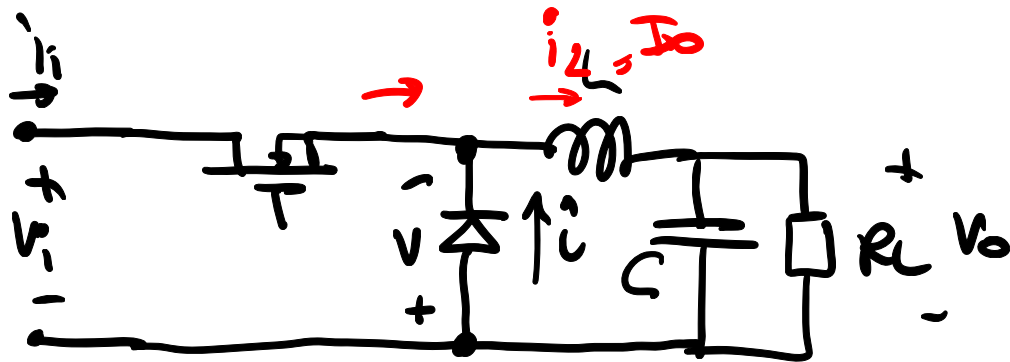
Soft switching $\left\{ \begin{array}{l} \rightarrow \text{Zero Current Switching} \quad \text{ZCS} \\ \rightarrow \text{Zero Voltage Switching} \quad \text{ZVS} \end{array} \right.$

DIODO

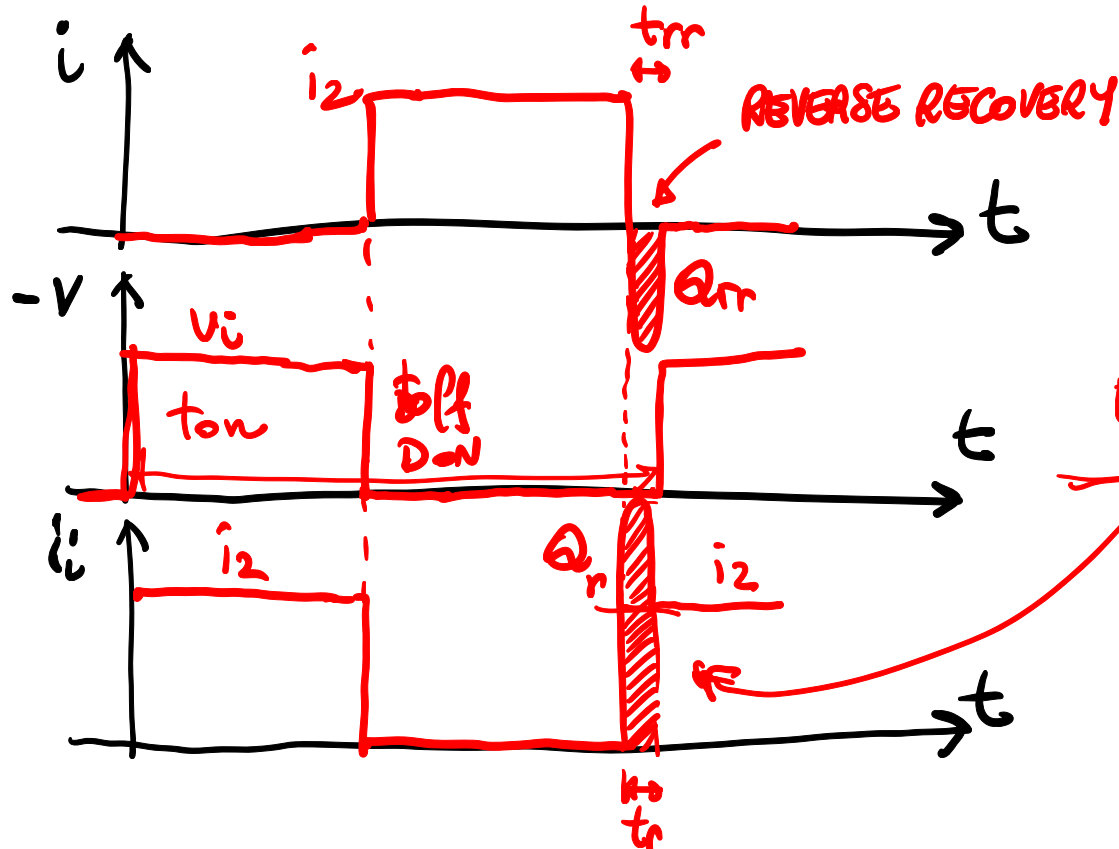
→ reverse recovery

Conduzione in inversa durante lo spegnimento

Es.



Hard Switching

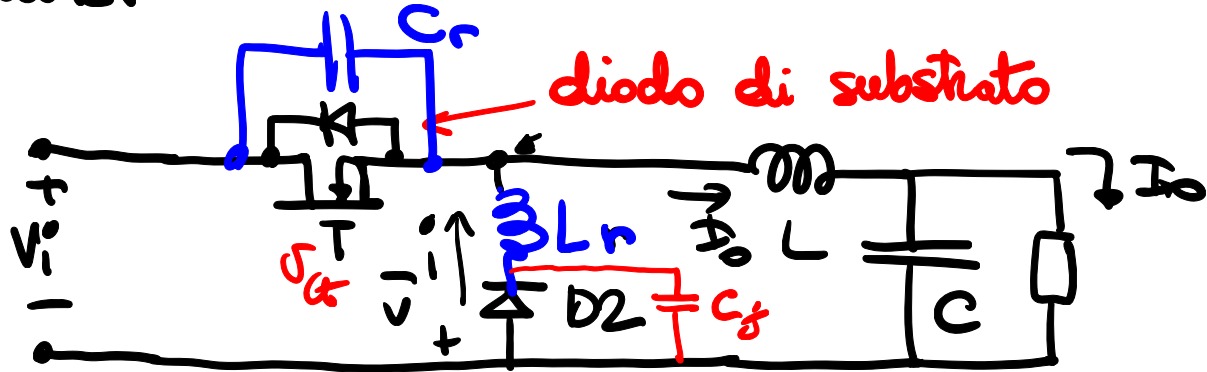


$$E = V_i \int i_D dt = V_i [t_{rr} I_D + Q_{rr}]$$

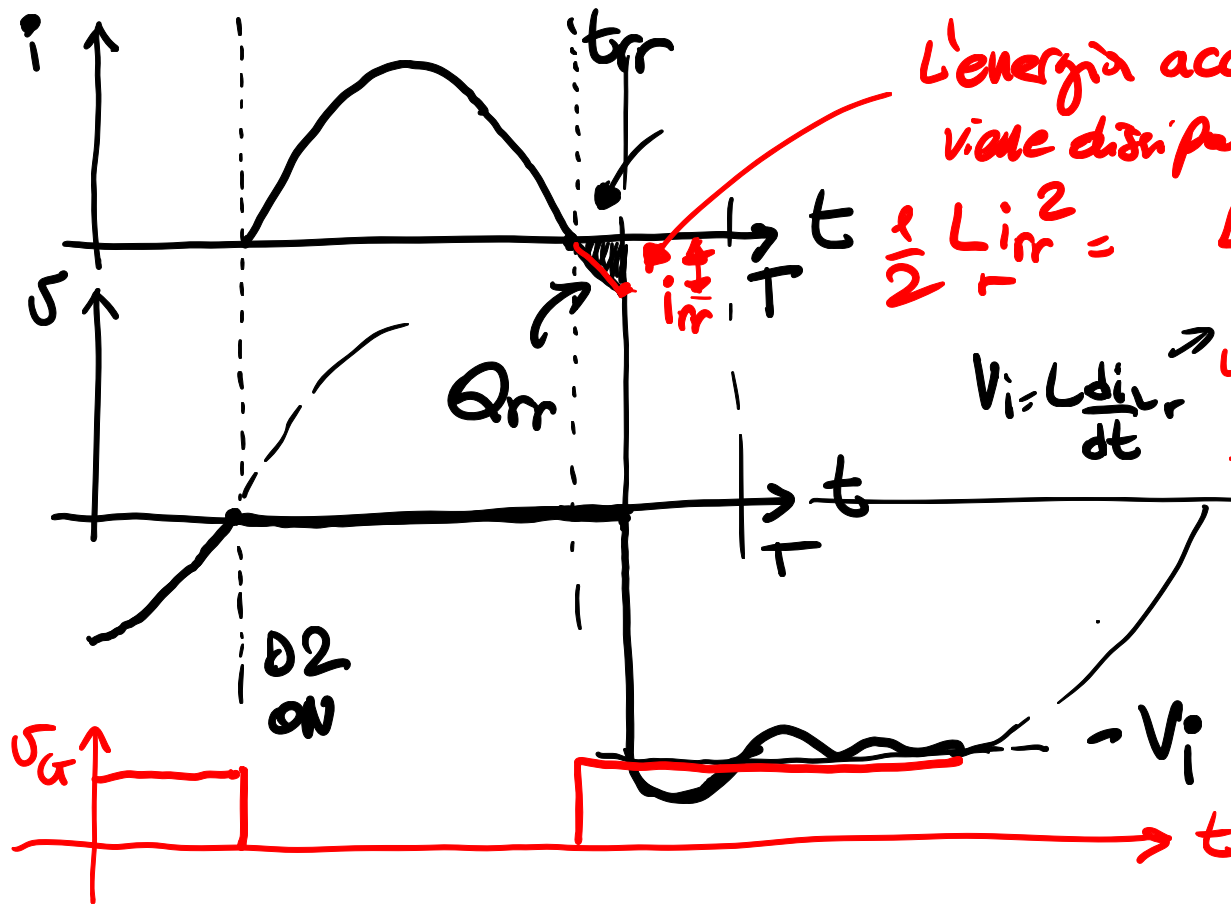
[trr]

↑ Energia persa nel diodo per ogni spegnimento

Quasi resonant ZCS buck



$$\frac{1}{2\pi\sqrt{L_r C_r}} \sim f_s$$

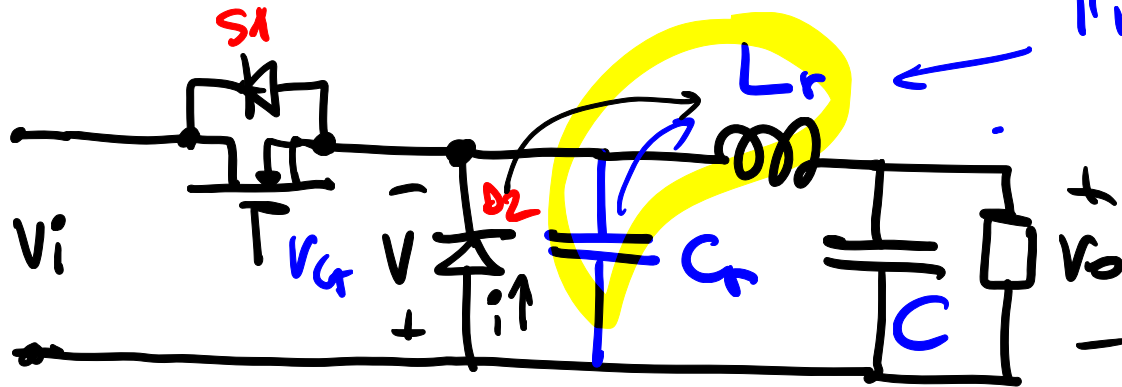


L'energia accumulata dall'induttore \$L_r\$ viene dissipata

$$\frac{1}{2} L i_{rr}^2 = \underbrace{L \left(\frac{i_{rr}}{t_{rr}} \right)}_{V_i} \underbrace{\frac{t_{rr} i_{rr}}{2}}_{Q_{rr}} = \underline{V_i Q_{rr}}$$

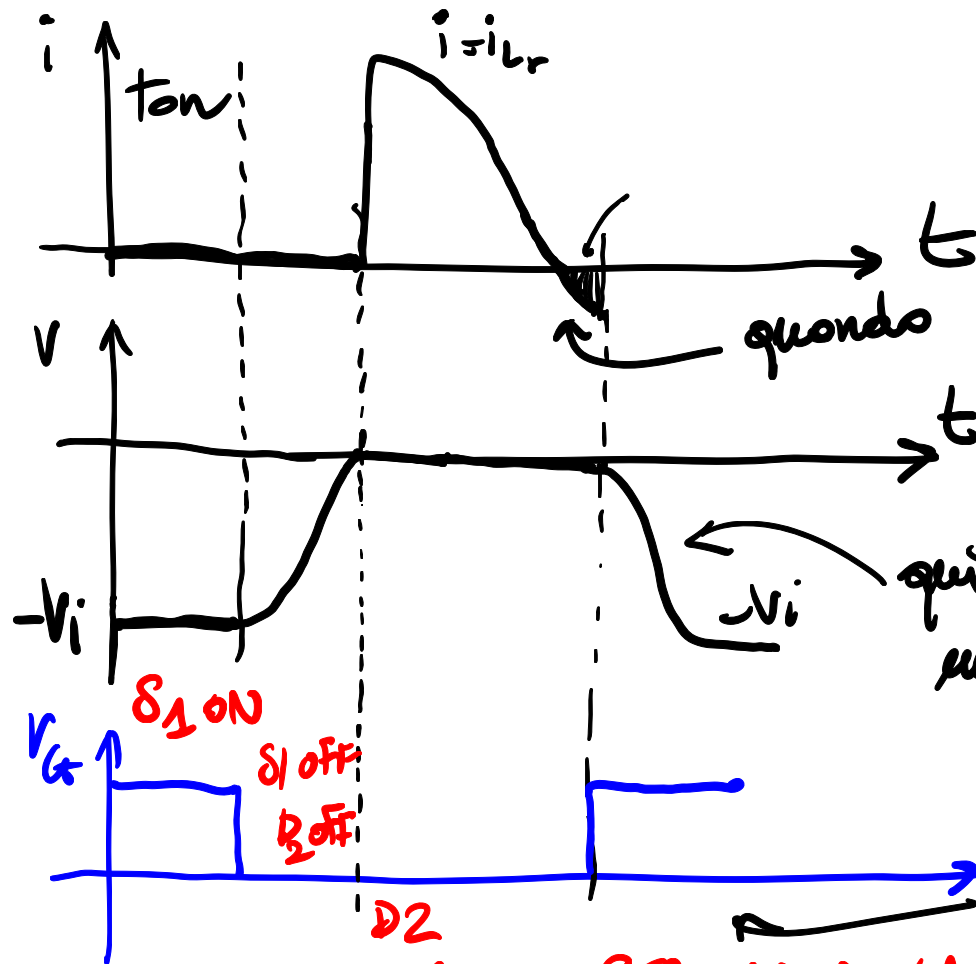
più piccolo che nel caso di Hard Switching perché la corrente varia più dolcemente

Quasi resonant ZVS buck



l'induttanza del filtro
risona con Cr

il diodo viene spento
da Lr



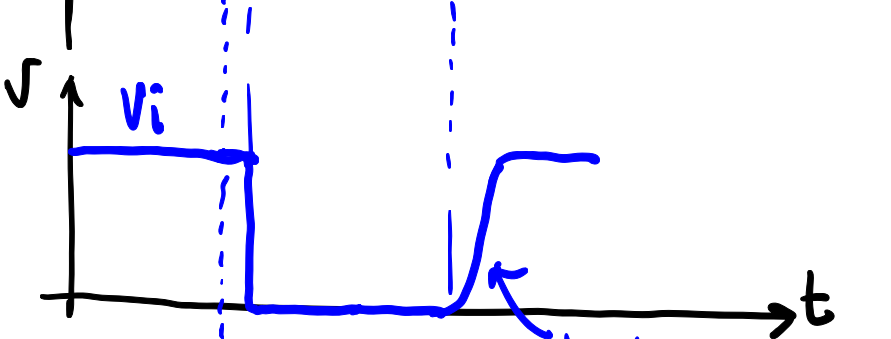
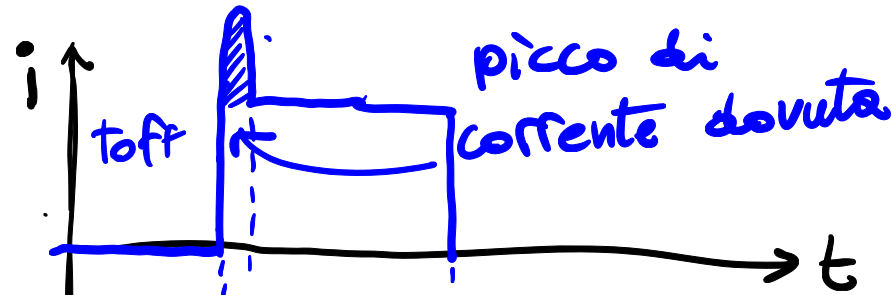
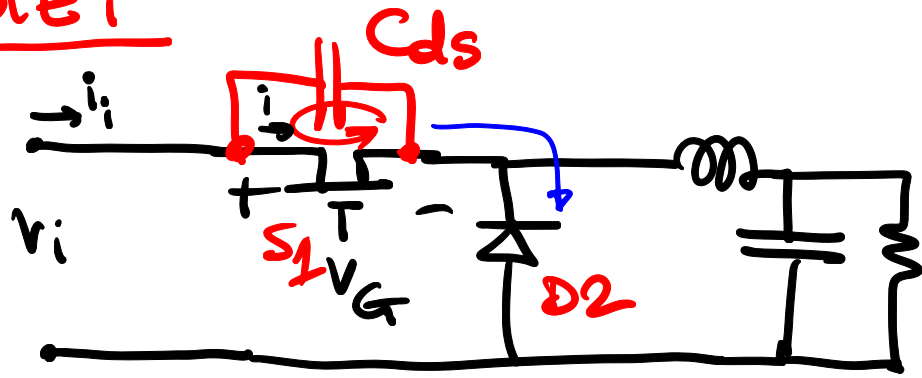
quando la corrente nel diodo è
negativa la tensione sul
diodo è nulla

qui il diodo si comporta come
una capacità (variabile) in
parallelo a Cr

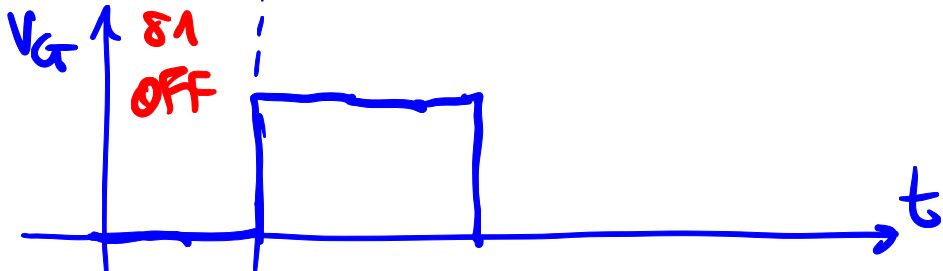
PERDITE IDEALMENTE NULLE

PER UN DIODO LA CONDIZIONE IDEALE È LO SPEGNIMENTO
ZVS

MOSFET



D2 ON
S1 OFF



picco di corrente dovuta alla I_{rr} (reverse recovery del diodo) e alla scarica della C_{ds}

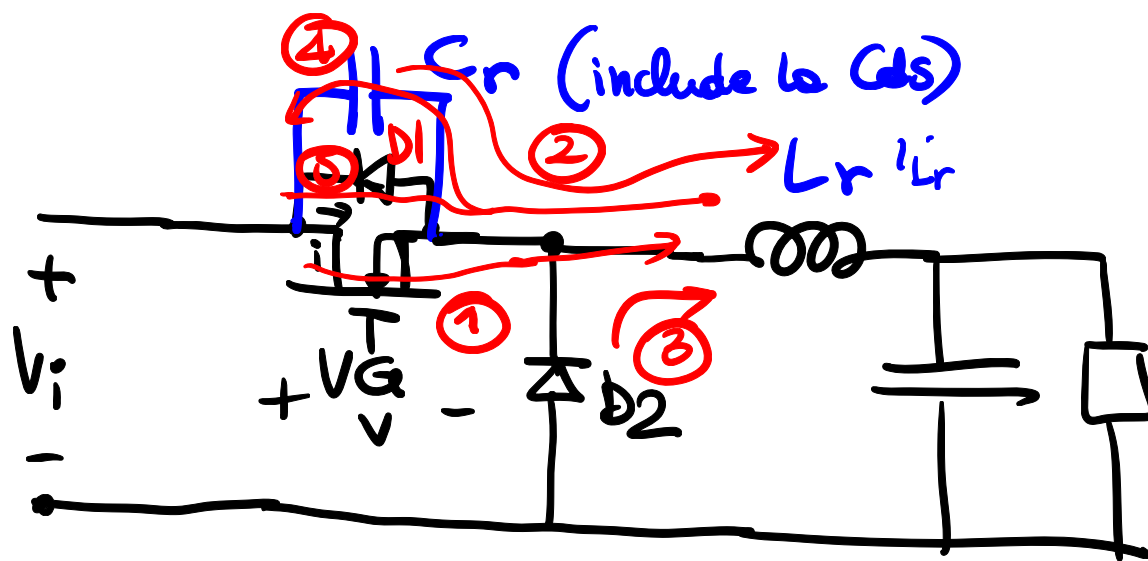
ENERGIA C_{ds}
 $\frac{1}{2} C_{ds} V_i^2$

ENERGIA DIONO $V_i [Q_{rr} + I_{D,rr}]$

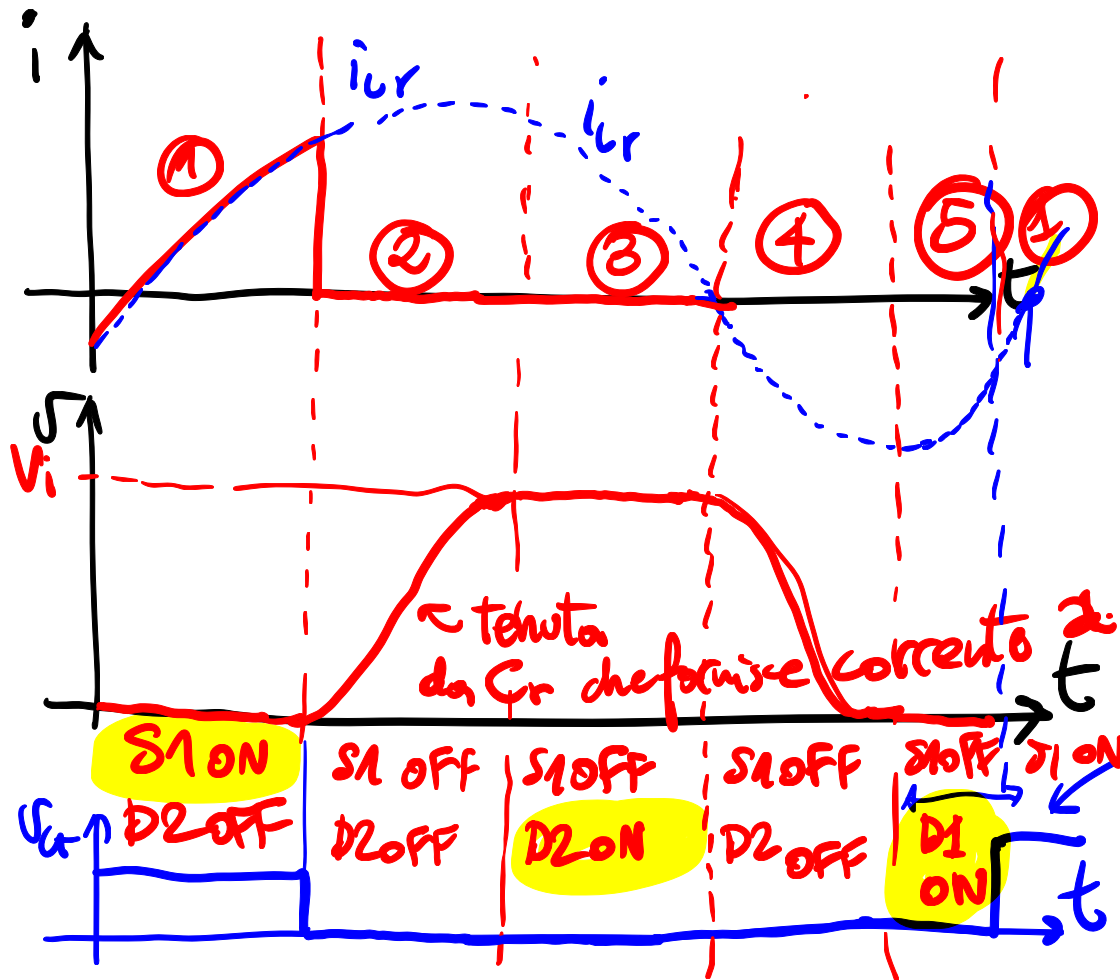
PERDITA DI ACCENSIONE
 IMPORTANTE

MI SERVE UNO ZV

ZVS



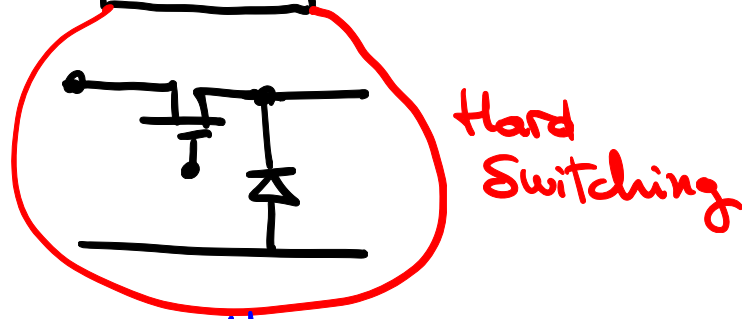
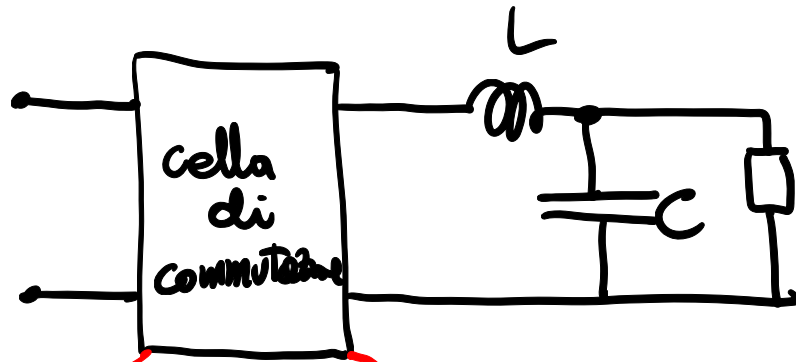
- ① S1 dà i_{Lr}
- ② C_r dà i_{Lr}
- ③ D2 " "
- ④ C_r " "
- ⑤ D1 " "



ACCENDIAMO S1
 QUANDO D1 conduce
 quindi $V_{DS} = 0$

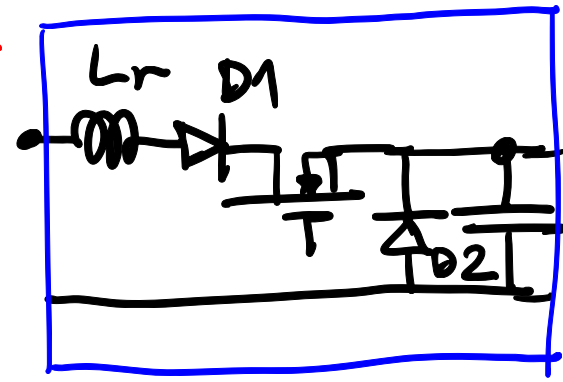
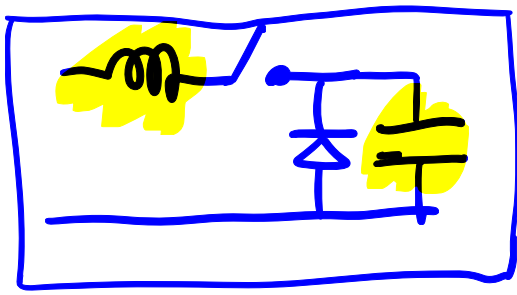
ZCS

Es. buck

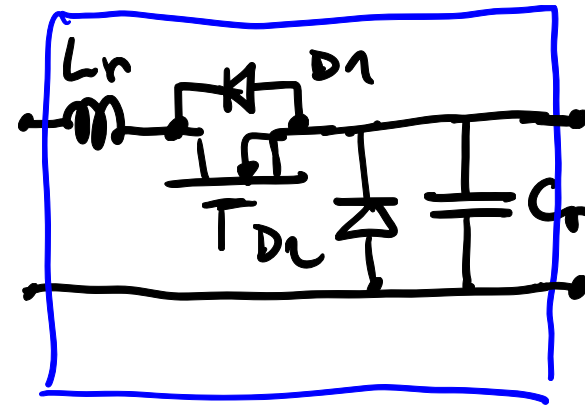


Hard Switching

cella quasi risonante



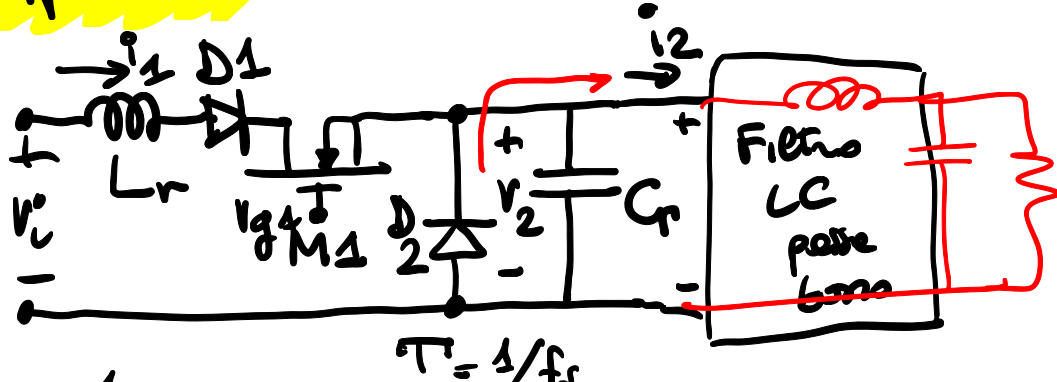
Half wave ZCS
Quasi Resonant
switch cell



Full wave ZCS
Quasi Resonant
switch cell

$$f_0 = \frac{1}{2\pi \sqrt{L_r C_r}} \approx f_s$$

Half wave ZCS QR switch cell



PER SEMPLICITÀ SUPPONIAMO i_2 costante
 Costante
 (trascuriamo il ripple in i_2)
 ($L \rightarrow \infty$)



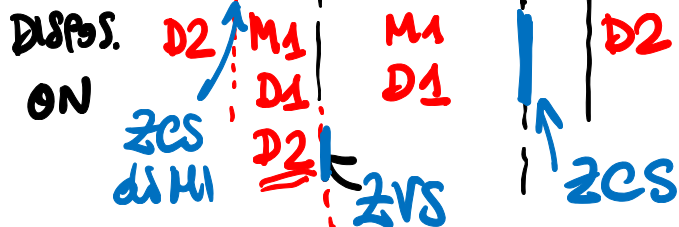
\Rightarrow a $t=0$ M_1 viene acceso, ma finché $i_1 < i_2$ il diodo D_2 rimane ON
 $\Rightarrow D_2$ si spegne quando $i_1 = i_2$



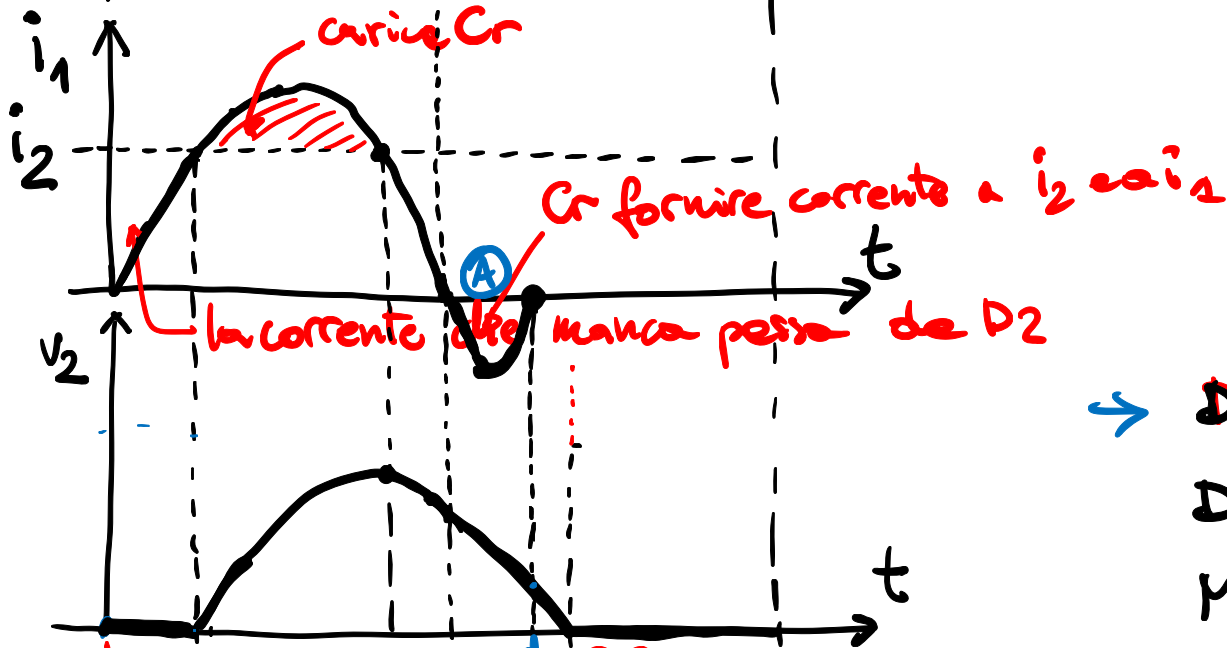
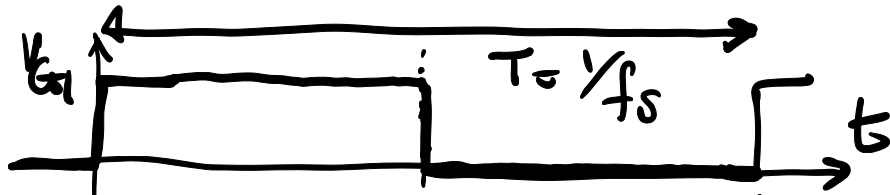
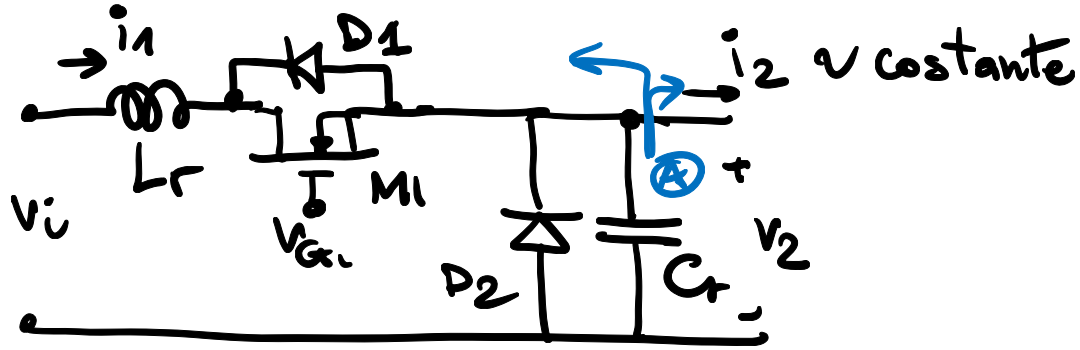
D2 : ZVS a cause di C_r che rallenta v_2

D1 : ZCS quando $i_1 = 0$ viene spento $M_1 \rightarrow D_1$

M_1 accensione in ZCS a causa di L_r



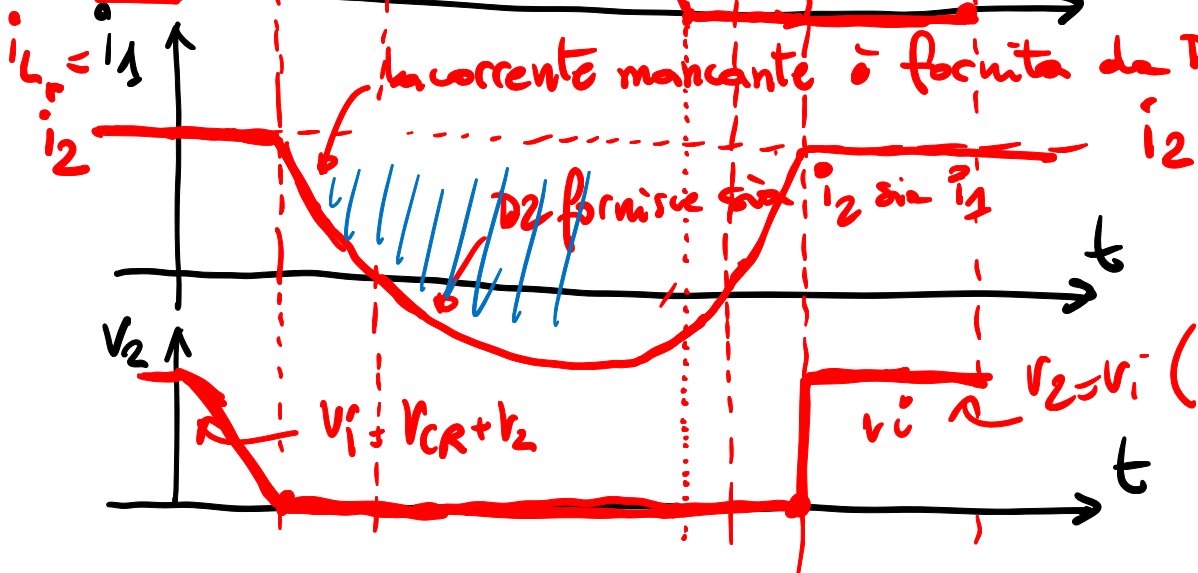
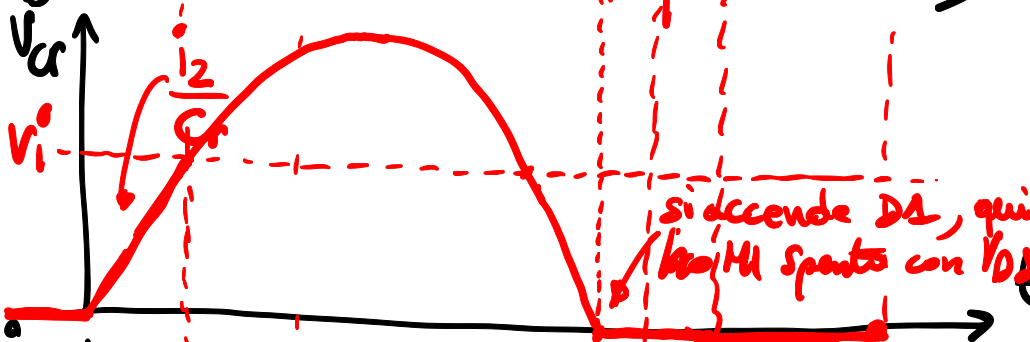
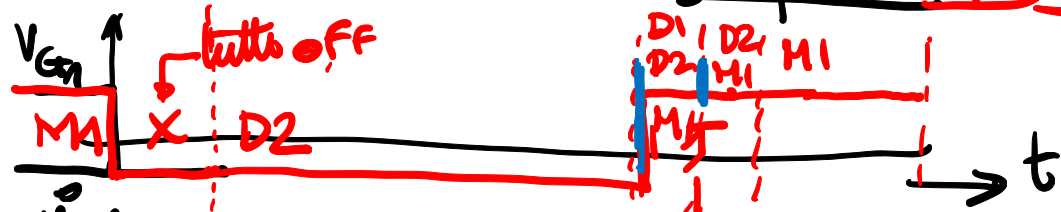
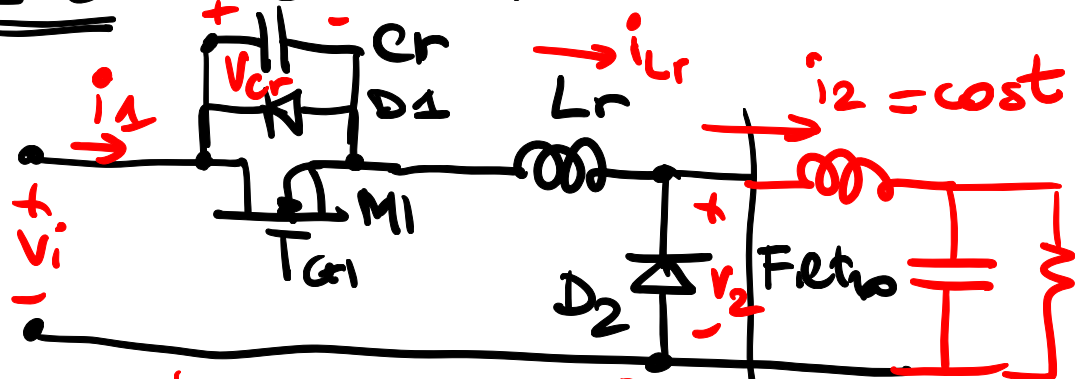
Full Wave ZCS Quasi resonant switch



- D2 spegnimento in ZVS (C_r)
- D1 spegnimento in ZCS
- M1 accensione in ZCS (L_r)

DISP. ON : D2 M1 M1 D1 D2
 ZVS tutto OFF ZCS

ZVS QUASI RESONANT Switch cell

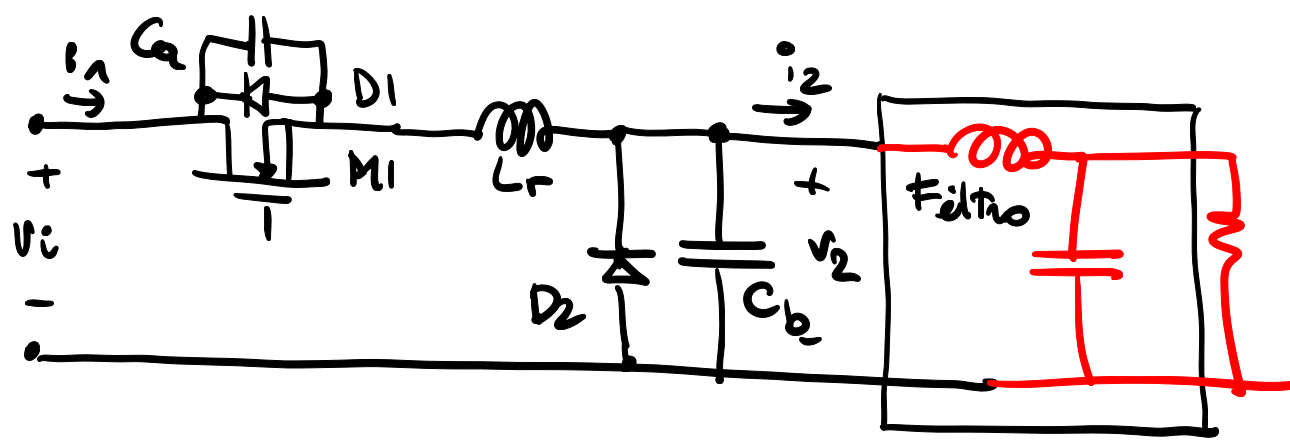


1) quando spegniamo M1, D2 non accende perché C_r rallenta la salita di V_{cr} [e quindi la discesa di v₂]

2) D2 rimane acceso fintanto che i₁ < i₂

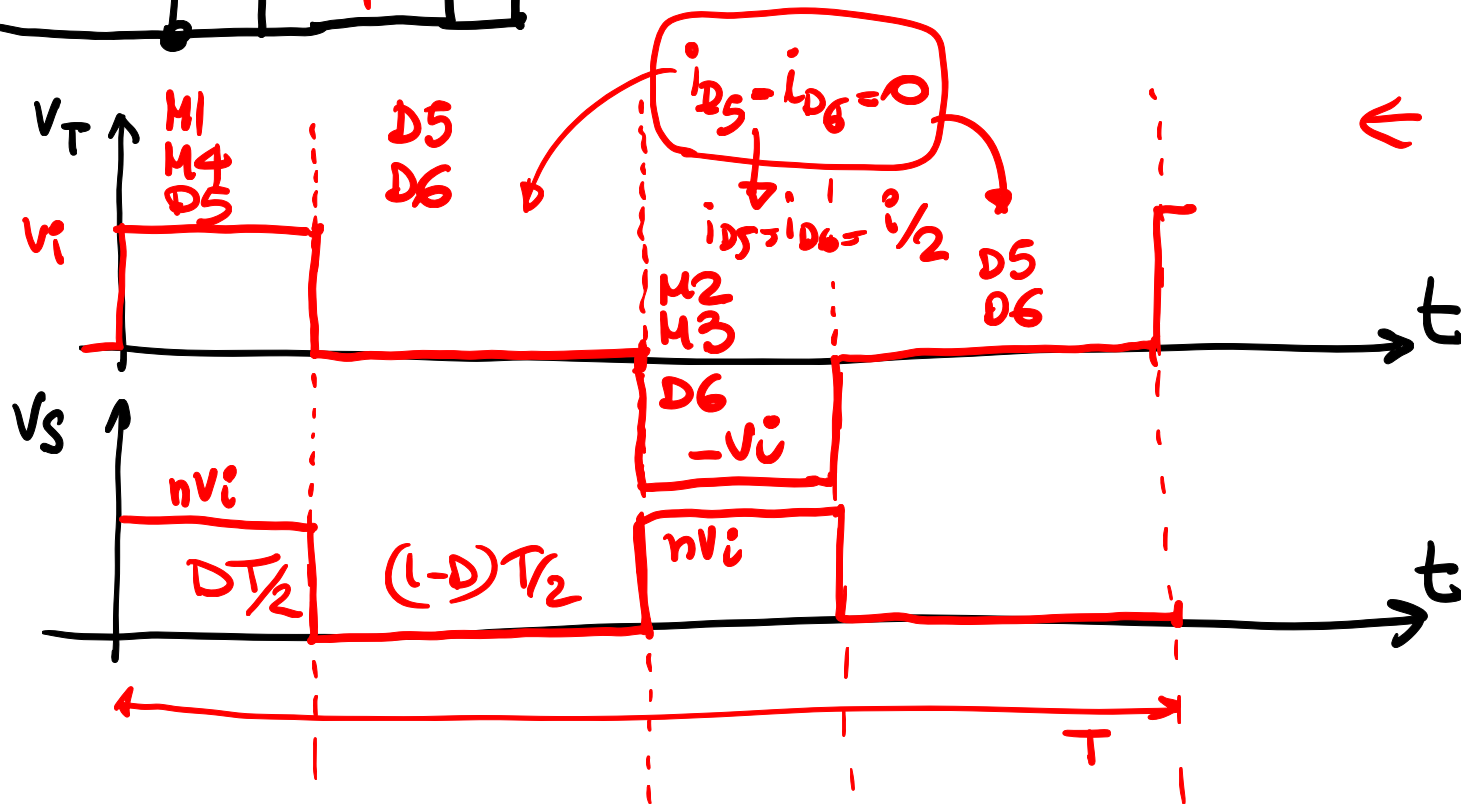
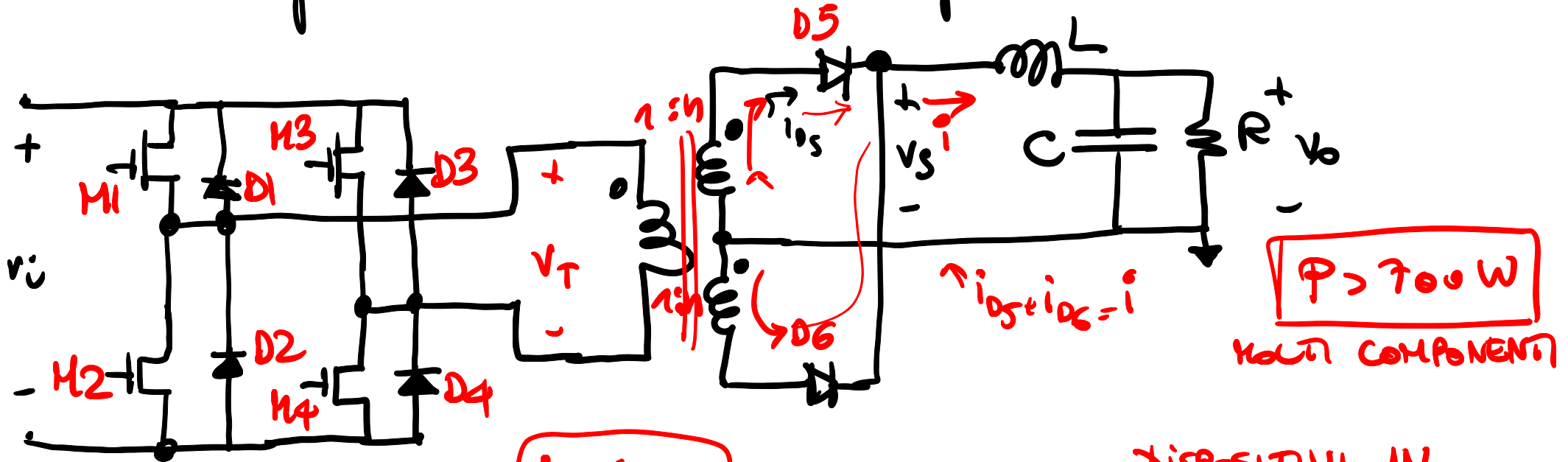
(le condotte se L_r è nulla e M1 è ON)

- || M1: ZVS in accensione (consentito da D1)
- || D1: ZVS in spegnimento (consentito da D1)
- || D2: ZCS in spegnimento



- D_2 : ZVS in spegnimento [consentito da C_b]
- M_1 : ZVS in accensione [le V_{os} è tenuta a zero da D_1 in conduzione]
- D_1 : ZVS in spegnimento [le V_o è tenuta a zero da M_1 in conduzione]

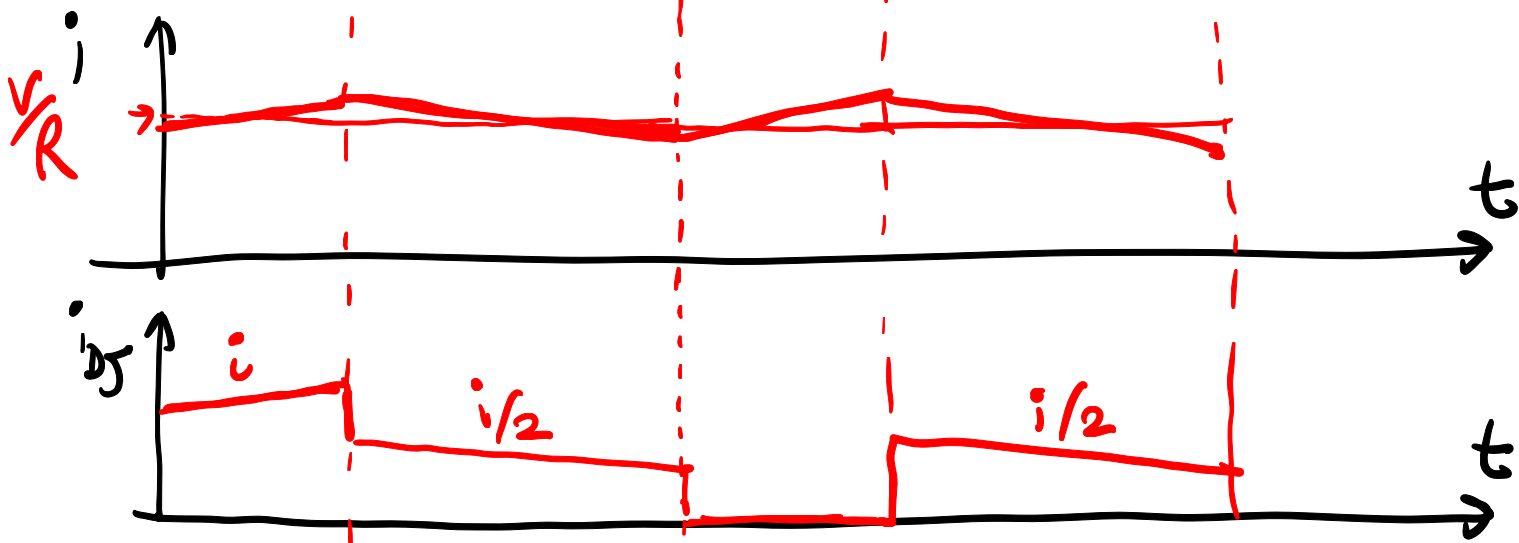
Full Bridge con isolamento a trasformatore



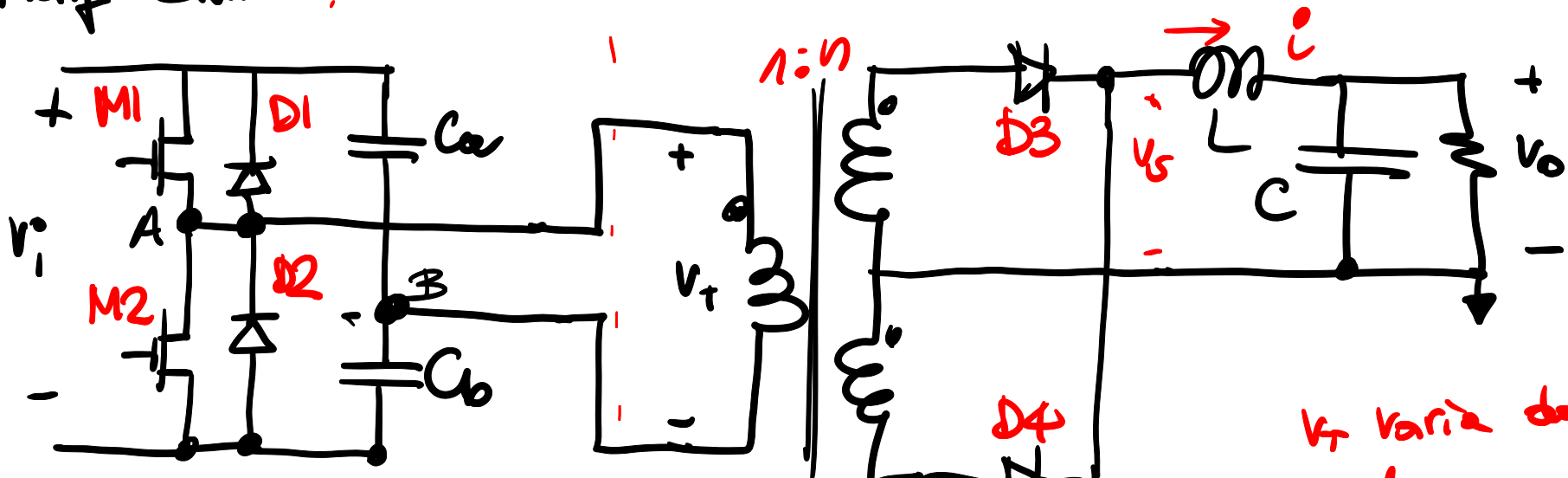
DISPOSITIVI IN CONDUZIONE

$$V_o = DnV_i$$

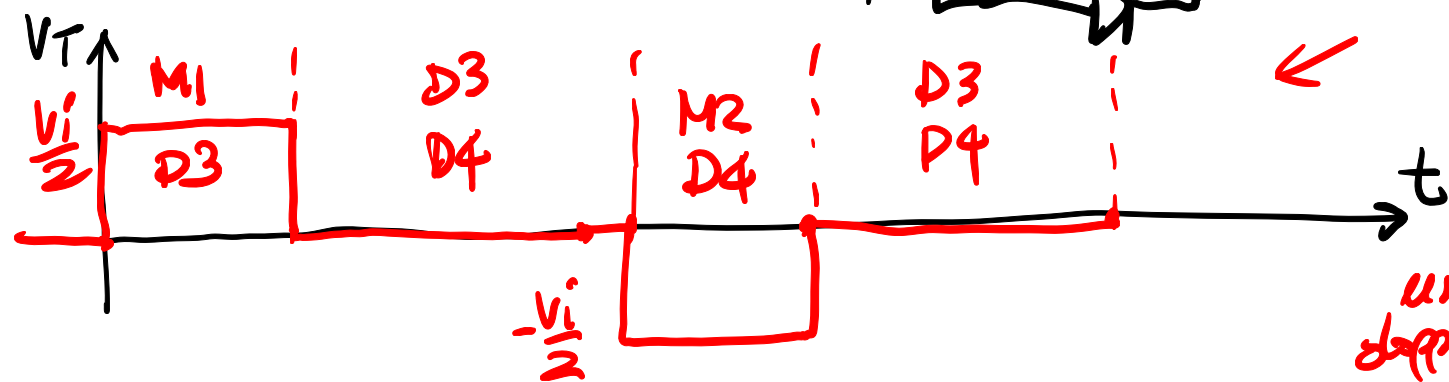
$$\frac{V_o}{V_i} = Dn$$



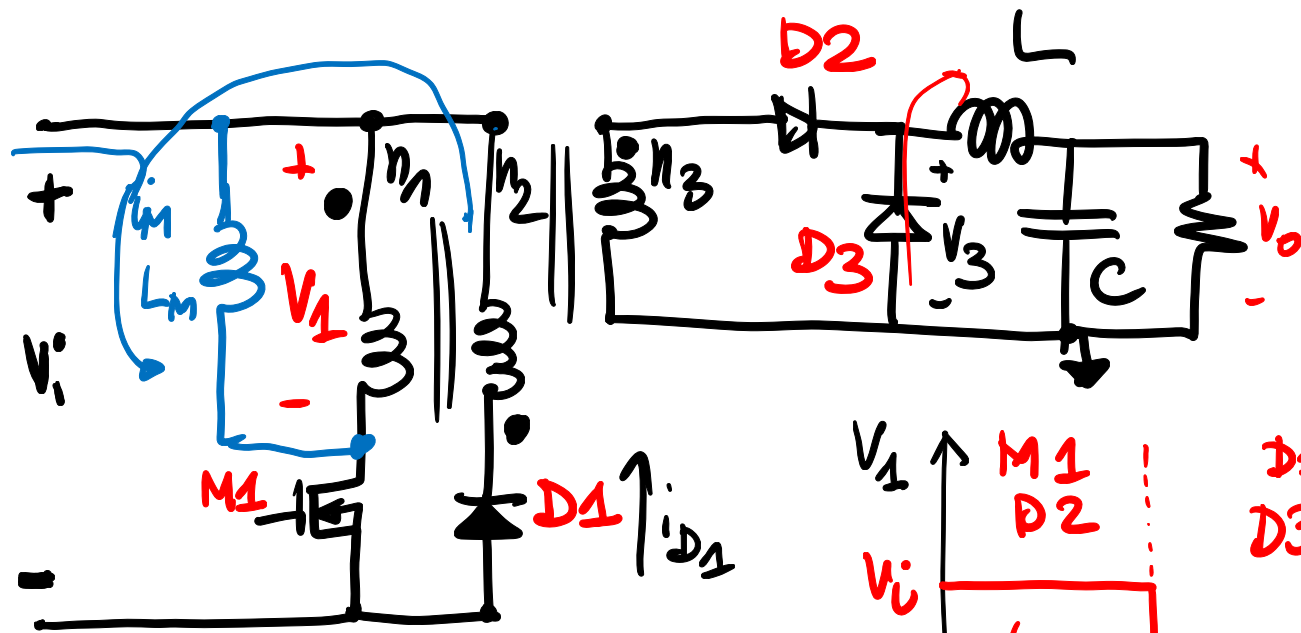
Half BRIDGE con ISOLAMENTO A TRASFORMATORE



v_T varia da $+\frac{v_i}{2}$ e $-\frac{v_i}{2}$
 ↳ posso compensare raddoppiando n
 ↳ e parte di potenza in uscita ha una corrente doppia sul primario



FORWARD CONVERTER

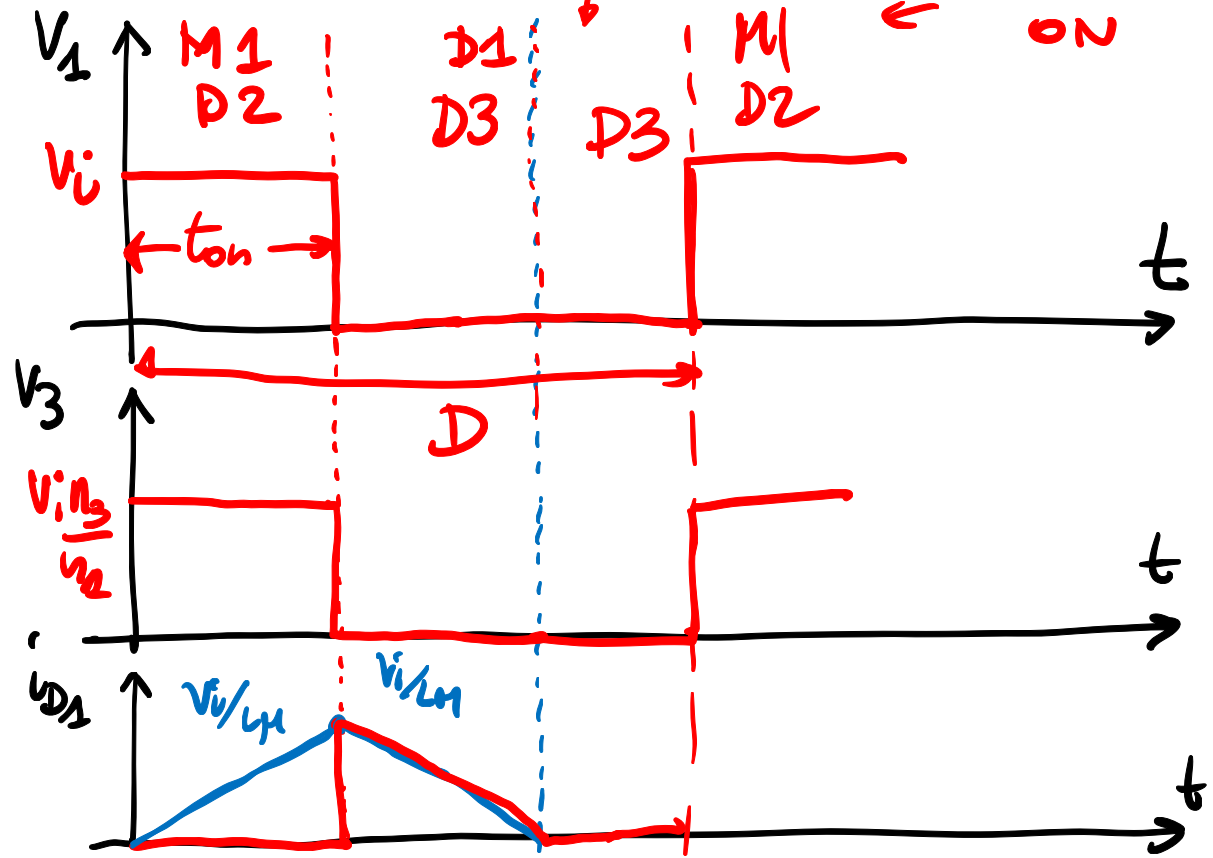


se $n_1 = n_2 \rightarrow D < \frac{1}{2}$

Facciamo questa

tutti of ipotesi

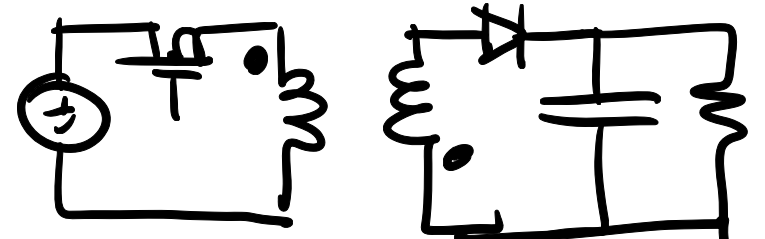
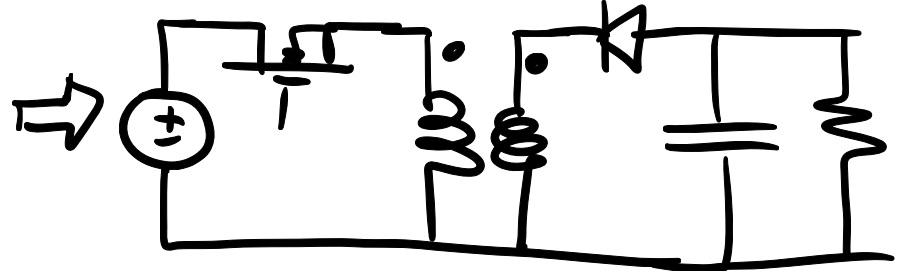
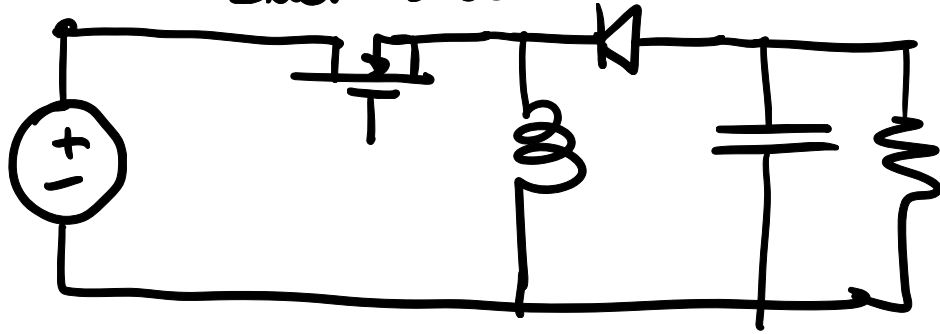
DISPOSITIVI ON



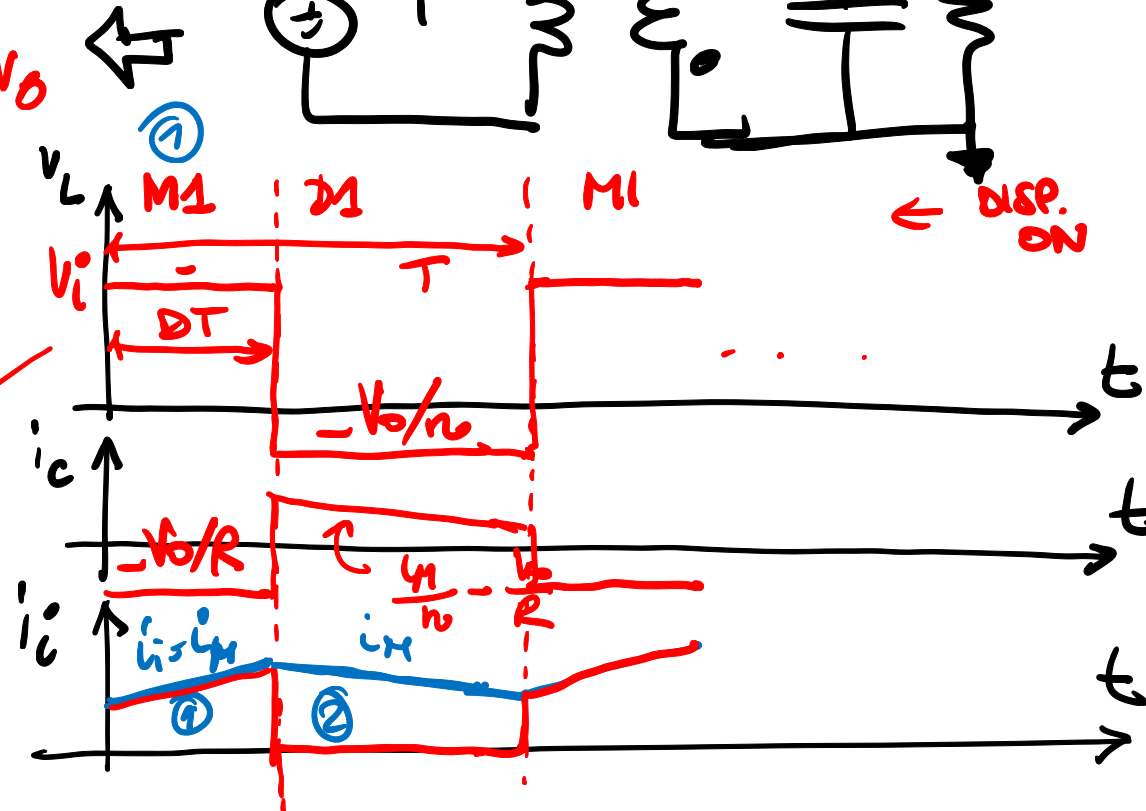
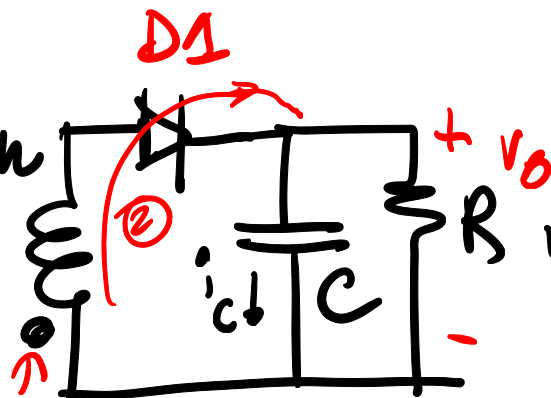
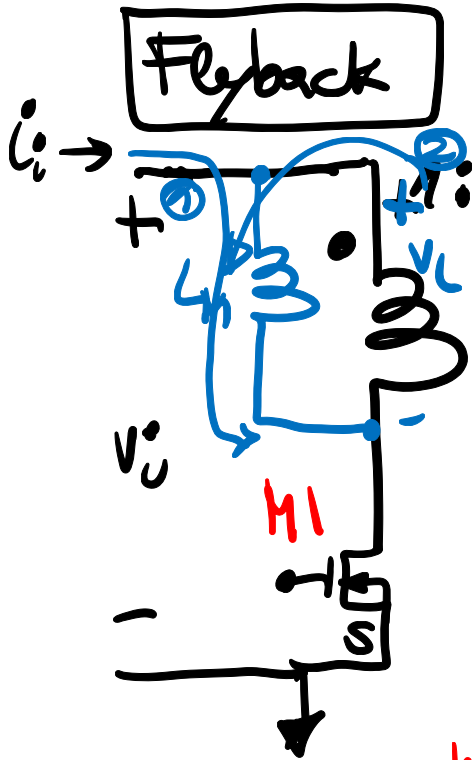
$$V_o = D V_i \left(\frac{n_3}{n_1} \right)$$

FLYBACK (basato sull'architettura buck boost)

Buck-boost



← DISP. ON

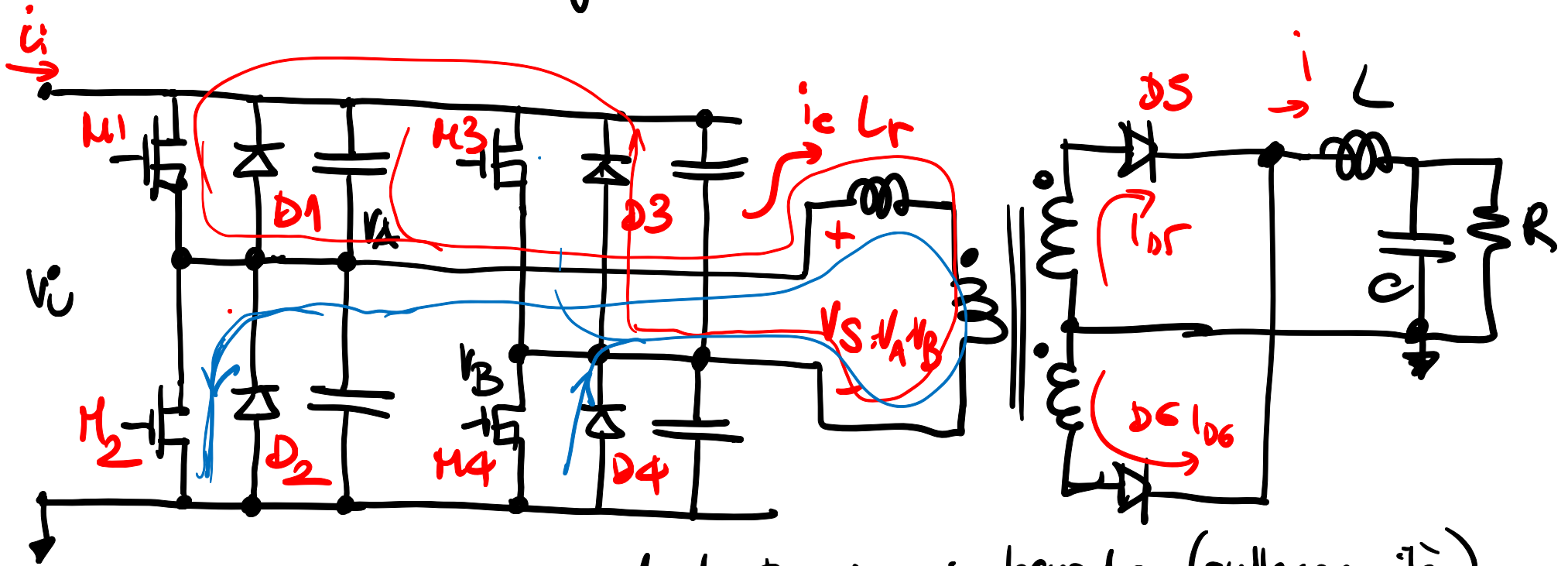


$$\langle v_L \rangle = 0$$

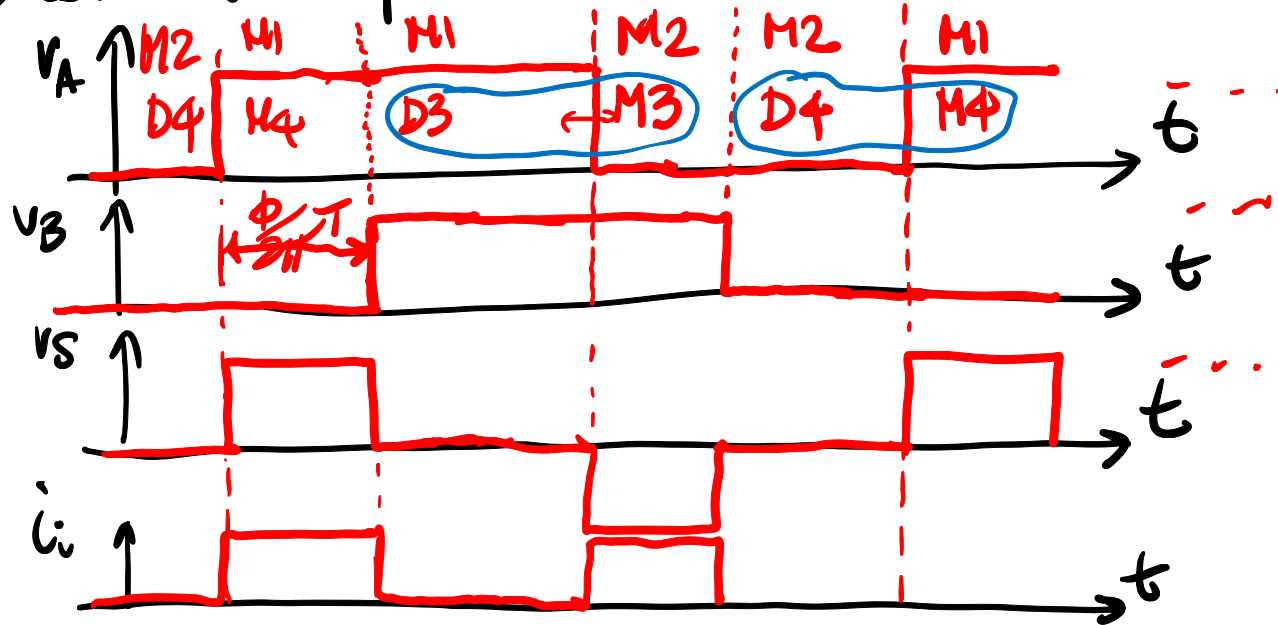
$$v_i D T - \frac{v_o}{n} (1-D) T = 0$$

$$\frac{v_o}{v_i} = \frac{n D}{1-D}$$

ZVS in Full Bridge con accoppiamento e Trasformatore



Consideriamo per il momento le transizioni brusche (sulle capacità)



$$\frac{V_o}{V_i} = \left(\frac{\phi}{\pi} \right) n$$

$\frac{\phi}{\pi}$ el posto di D'

