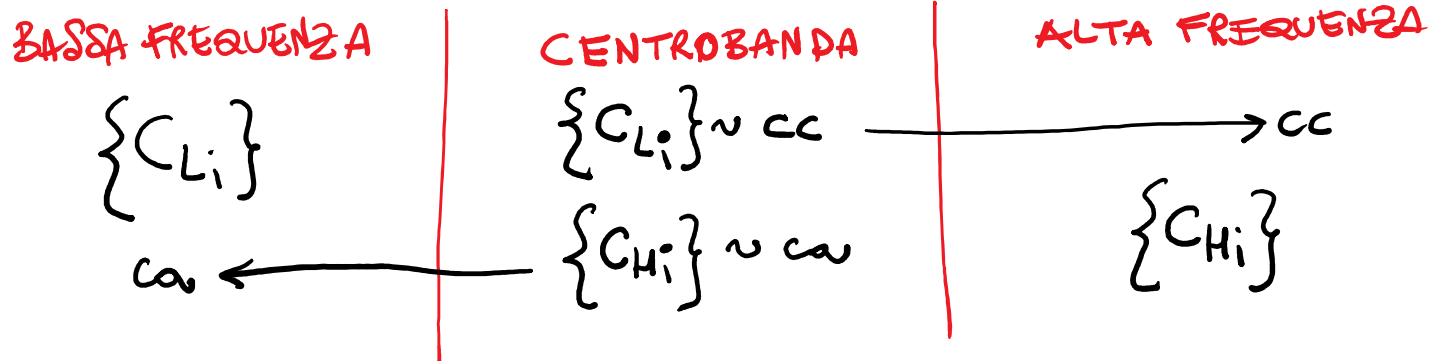


Comportamento in frequenza degli amplificatori

Wednesday, March 29, 2017 2:00 PM

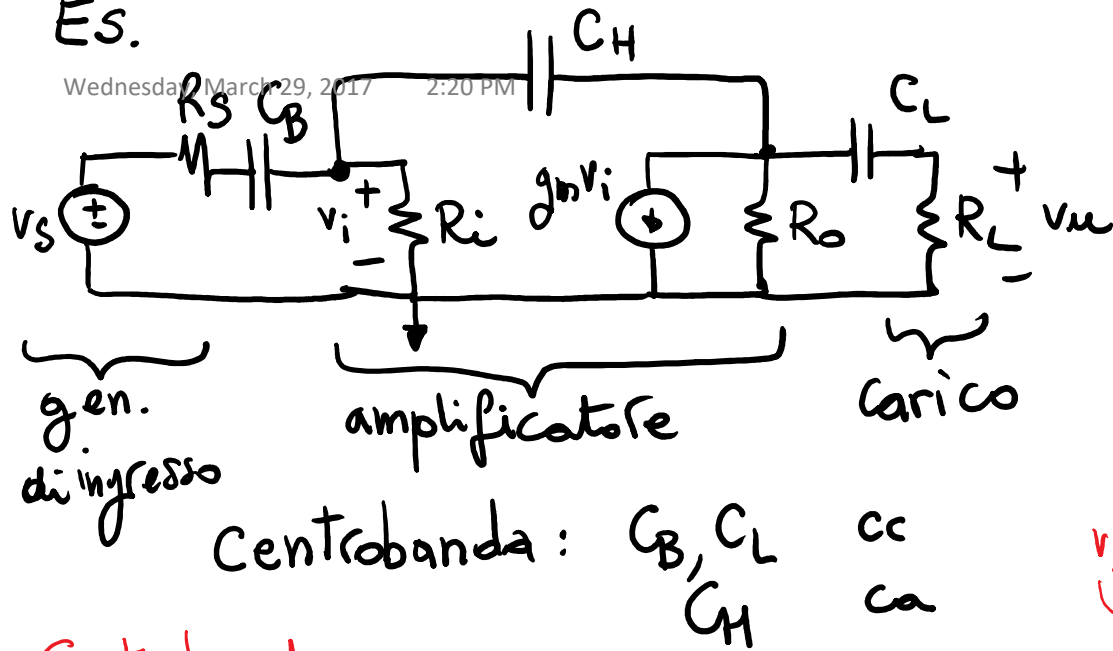
3) dobbiamo tenere conto dell'effetto di C e L
↑

CENTROBANDA: l'intervallo di frequenza in cui
 $|H(f)|$ NON DIPENDE DALLA FREQUENZA
[$H(f)$ è RESISTIVA]

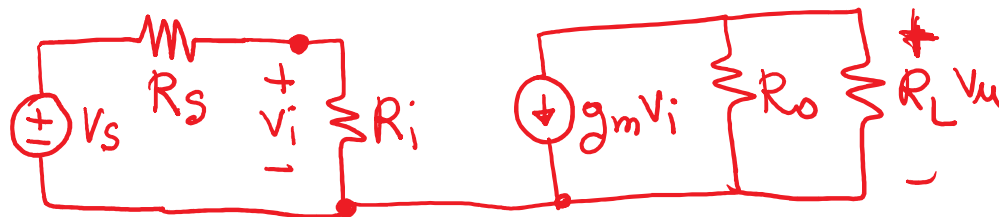


Es.

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Centrobanda



$$v_i = v_s \frac{R_i}{R_i + R_s}$$

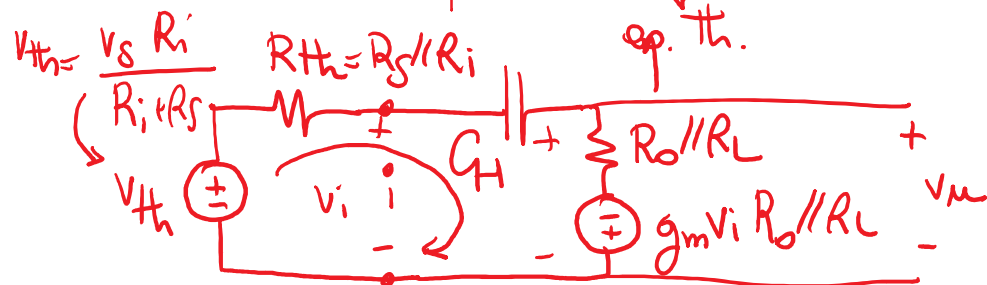
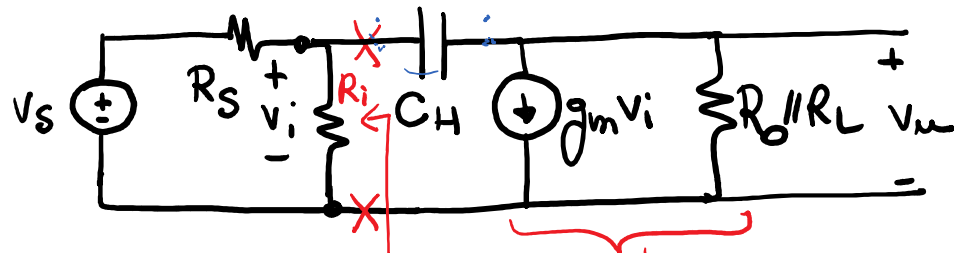
$$v_u = g_m v_i (R_o \parallel R_L)$$

$$A_{CB} = \frac{v_u}{v_s} = \frac{-g_m (R_o \parallel R_L) R_i}{R_i + R_s}$$

ALTA FREQUENZA

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C_H , C_L , C_B sono cc



eq. maglia : $V_{th} + g_m v_i R_o || R_L = i \left[R_{th} + R_o || R_L + \frac{1}{C_H s} \right]$

$v_i = V_{th} - R_{th} i$

$v_u = R_o || R_L i - g_m v_i R_o || R_L$

$$\begin{cases} v_{th} + g_m (R_o \parallel R_L) (v_{th} - R_{th} i) = i \left[R_{th} + R_o \parallel R_L + \frac{1}{C_H s} \right] \\ v_u = R_o \parallel R_L i - g_m R_o \parallel R_L (v_{th} - R_{th} i) \end{cases}$$

$$\begin{cases} v_{th} (1 + g_m R_o \parallel R_L) = i \left[R_{th} + g_m (R_o \parallel R_L) R_{th} + R_o \parallel R_L + \frac{1}{C_H s} \right] \\ v_u = -g_m R_o \parallel R_L v_{th} + i \left[R_o \parallel R_L + g_m (R_o \parallel R_L) R_{th} \right] \end{cases}$$

$$\frac{v_u}{v_{th}} = \underbrace{-g_m R_o \parallel R_L} + \left[\frac{(1 + g_m R_o \parallel R_L)}{R_{th} + \frac{1}{C_H s}} \right] \left[R_o \parallel R_L + g_m (R_o \parallel R_L) R_{th} \right]$$

$$A_H = \frac{v_u}{v_s} = \frac{v_u}{v_{th}} \cdot \frac{v_{th}}{v_s} = A_{H0} \frac{(1 - s/s_2)}{(1 - s/s_1)}$$

↑
FdT in ALTA FREQUENZA

$$A_{H0} = \lim_{s \rightarrow 0} A_H = \left[-g_m R_o \parallel R_L \left(\frac{R_i}{R_i + R_s} \right) \right] = A_{CB}$$

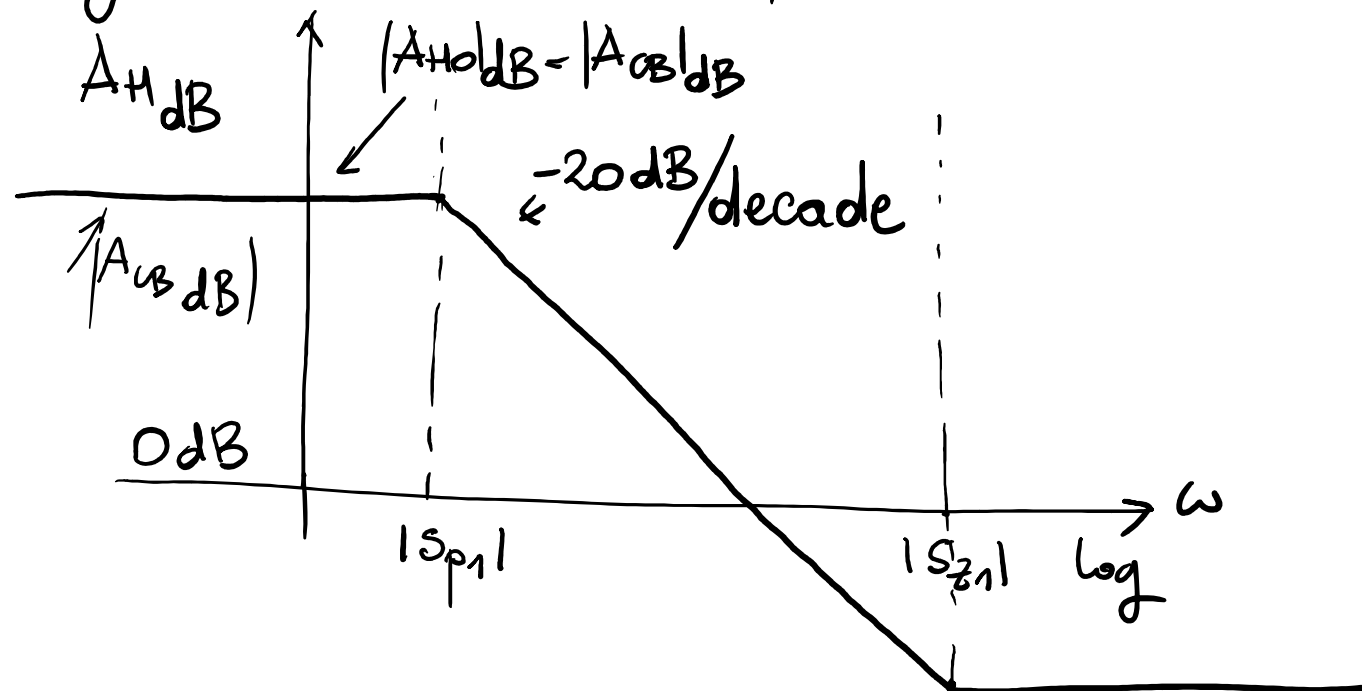
$$\underline{s_{p1}} : R_H + \frac{1}{C_H s_{p1}} = 0 \Rightarrow \boxed{s_{p1} = -\frac{1}{R_H C_H}}$$

$$\lim_{s \rightarrow \infty} A_H = A_{H\infty} = A_{H0} \frac{s_{p1}}{s_{z1}} \Rightarrow \boxed{s_{z1} = \frac{A_{H0} s_{p1}}{A_{H\infty}}}$$

Diagramma di Bode di ampiezza

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2:54 PM

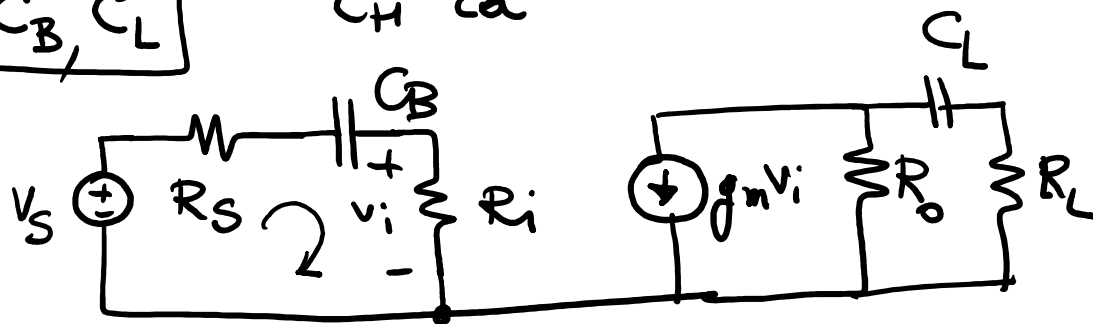


BASSA FREQUENZA

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C_B, C_L

C_H ca



$$\frac{v_i}{V_S} = \frac{R_i}{R_i + R_S + \frac{1}{C_B S}} = \frac{R_i C_B S}{1 + (R_i + R_S) C_B S}$$



$$v_u = -g_m v_i R_o \frac{R_L}{R_L + R_o + \frac{1}{C_L S}}$$

$$\frac{v_u}{v_i} = \frac{-g_m R_o R_L C_L S}{(R_i + R_o) C_L S + 1}$$

$$A_L = \frac{v_u}{v_s} = \frac{v_u}{v_i} \cdot \frac{v_i}{v_b} = \frac{-g_m R_L R_o C_L s}{1 + (R_L + R_o) C_L s} \cdot \frac{R_i C_B s}{1 + (R_i + R_s) C_B s}$$

2 poli reali NEGATIVI

2 zeri nell'origine

$$s_{p2} = \frac{-1}{(R_L + R_o) C_L}$$

$$s_{p3} = \frac{-1}{(R_i + R_s) C_B}$$

$$\lim_{s \rightarrow \infty} (A_L) = -g_m \overbrace{\left(\frac{R_L \cdot R_o}{R_L + R_o} \right)}^{R_L \parallel R_o} \frac{R_i}{R_i + R_s} = A_{CB}$$

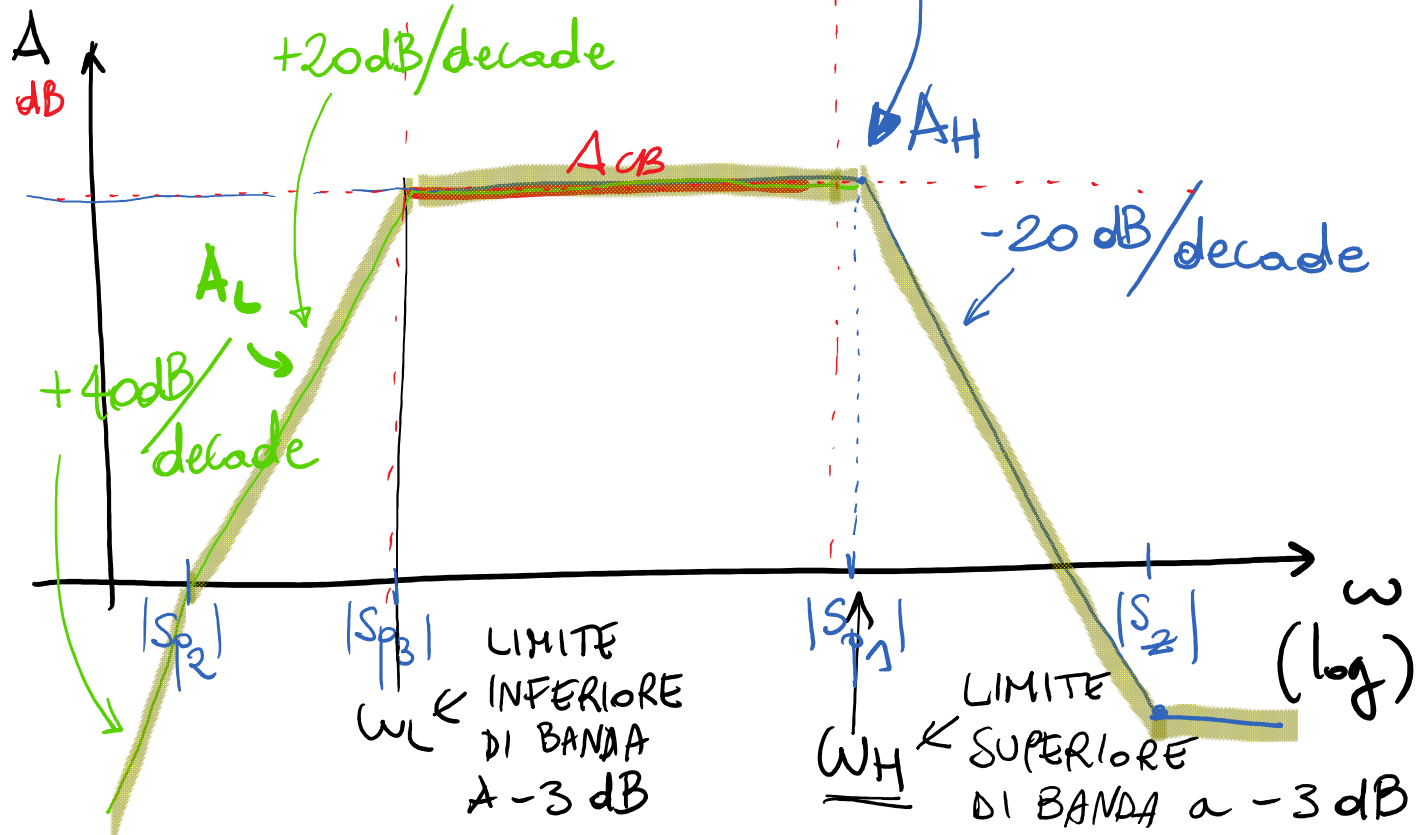
LF

CB

HF

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3:08 PM



METODO DI COCHRAN-GRABEL

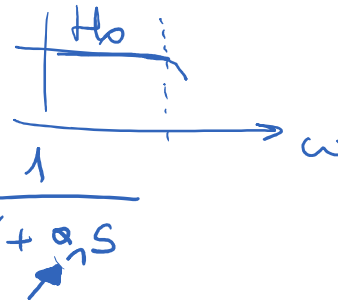
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X CALCOLARE TUTTI I COEFFICIENTI DELLA
FUNZIONE DI TRASFERIMENTO DI UN CIRCUITO
CON R, C, generatori controllati
in funzione delle capacità e di alcune resistenze viste

$$H(s) = H_0 \frac{1 + b_1 s + b_2 s^2 + \dots + b_n s^n}{1 + a_1 s + a_2 s^2 + \dots + a_n s^n} \quad \leftarrow \text{Espressione Passa Basso}$$

Espansione al 1° ORDINE IN (s)

$$\lim_{s \rightarrow 0} H(s) = H_0 \quad H(s) = H_0 \frac{1 + b_1 s}{1 + a_1 s} \sim H_0 \frac{1}{1 + a_1 s}$$



LIMITE SUPERIORE DI BANDA A -3dB

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$$\omega_H \rightarrow |H(j\omega_H)| = \frac{H_0}{\sqrt{2}}$$

$$\left| \frac{H_0}{1+j\omega_H a_1} \right| = \frac{H_0}{\sqrt{2}} \rightarrow a_1 \omega_H = 1$$

$$\omega_H = \frac{1}{a_1}$$

dal METODO di Cochran-GRABEL

$$a_1 = \sum_{i=1}^n R_i^o C_i$$

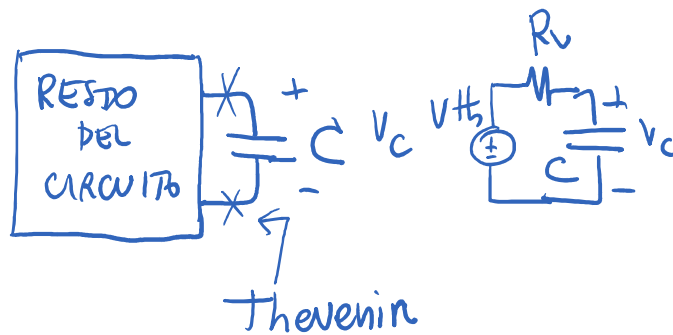
corrisponde su
tutte le capacità

RESISTENZA VISTA DA C_i
QUANDO TUTTE LE ALTRE
CAPACITÀ SONO UN CIRCUITO
APERTO

NEL CASO PARTICOLARE DI UNA SOLA CAPACITÀ

$$a_1 = R_V \dot{C} \rightarrow \omega_H = \frac{1}{R_V C} = |s_p|$$

↑
Resistenza
VISTA da C



$$V_C = V_{Th} \cdot \frac{\frac{1}{Cs}}{\frac{1}{Cs} + R_V} \Rightarrow \frac{V_C}{V_{Th}} = \frac{1}{1 + R_V Cs}$$

$$s_p = \frac{-1}{R_V C}$$

crd

FdT scritta in modo passa alto

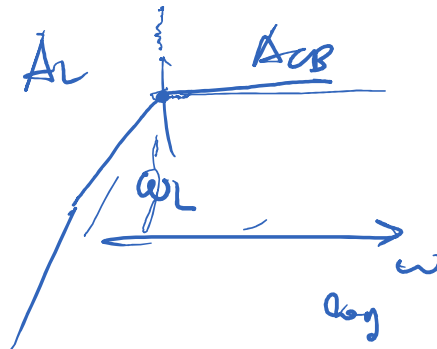
Wednesday, March 29, 2017 4:04 PM

$$H(s) = H_{\infty} \frac{s^n + d_{n-1}s^{n-1} + d_{n-2}s^{n-2} + \dots + d_0}{s^n + c_{n-1}s^{n-1} + c_{n-2}s^{n-2} + \dots + c_0}$$

$$\lim_{s \rightarrow \infty} H(s) = H_{\infty}$$

ESPANSIONE AL
1° ORDINE $\left(\frac{1}{s}\right)$

$$H(s) = H_{\infty} \frac{1 + d_{n-1}/s}{1 + c_{n-1}/s} \sim H_{\infty} \frac{1}{1 + c_{n-1}/s}$$



LIMITE INFERIORE DI BANDA

Wednesday, March 29, 2017 4:10 PM

A - 3dB

$$\omega_A \rightarrow |H(j\omega)| = \frac{|H_0|}{\sqrt{2}}$$

$$\left| H_0 \frac{1}{1 + \frac{C_{n-1}}{j\omega}} \right| = \frac{|H_0|}{\sqrt{2}}$$

$$\frac{C_{n-1}}{\omega_L} = 1 \Rightarrow \boxed{\omega_L = C_{n-1}}$$

dal
METODO COCHRAN-GRABEL

$$\omega_L = C_{n-1} = \sum_i \left(\frac{1}{R_i \cdot C_i} \right)$$

RESISTENZA
VISTA DA C_i
QUANDO TUTTE LE
CAPACITÀ SONO IN CC

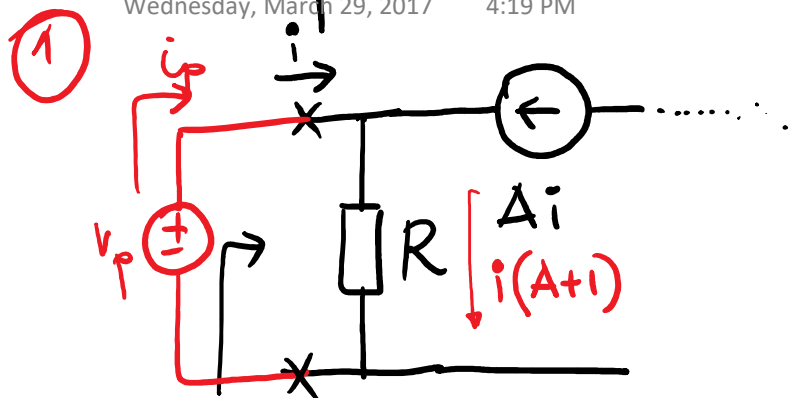
NUOVO ESEMPIO DI PRIMA

Wednesday, March 29, 2017 4:15 PM

$$C_{n-1} = C_1 = \frac{1}{C_B(R_S + R_i)} + \frac{1}{C_L(R_L + R_o)} \approx \omega_L$$

Casi tipici di RESISTENZE VISTE

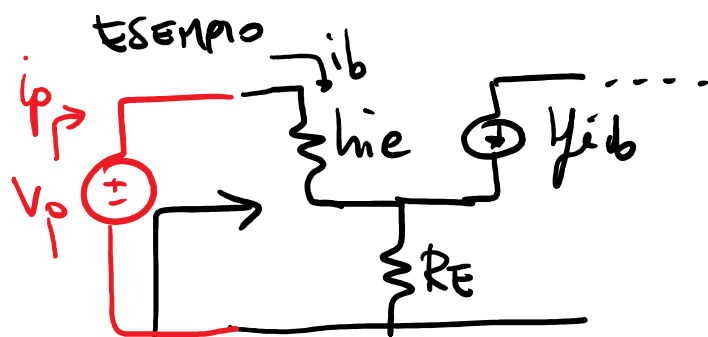
Wednesday, March 29, 2017 4:19 PM



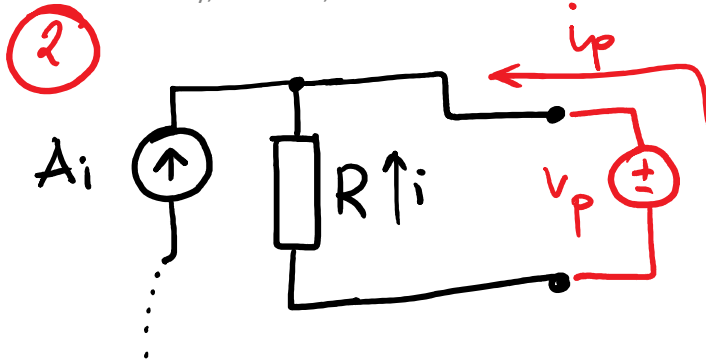
$$\bar{i}_p = i$$

$$V_p = R i (A+1)$$

$$R_v = \frac{V_p}{i_p} = \underline{\underline{R (A+1)}}$$



$$\underline{\underline{R_v = h_{ie} + R_E (\beta + 1)}}$$

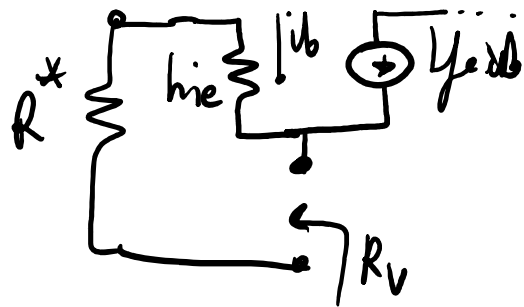


$$V_p = -R_i i_p$$

$$i_p = -i - A i$$

$$R_V = \frac{V_p}{i_p} = \frac{R}{A+1}$$

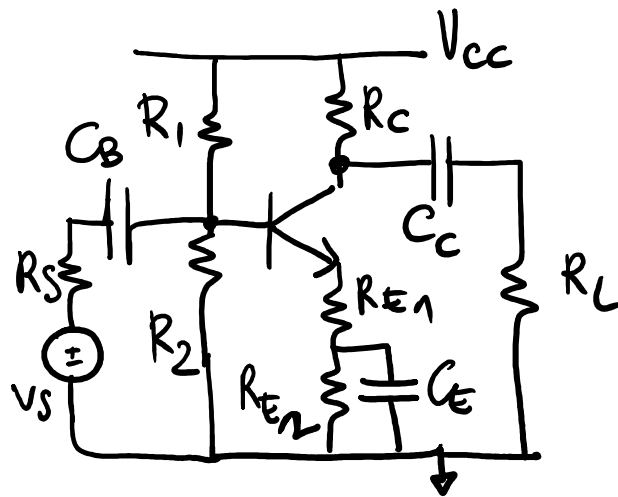
ESEMPIO



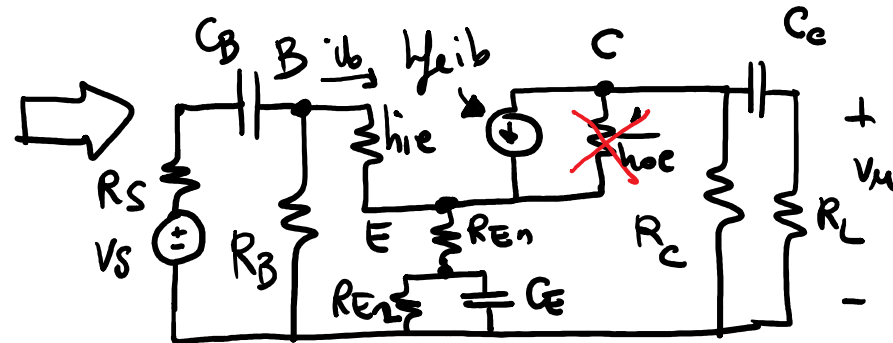
$$R_V = \frac{h_{ie} + R^*}{h_{fe} + 1}$$

Limite inferiore di banda

Wednesday, April 12, 2017 1:58 PM

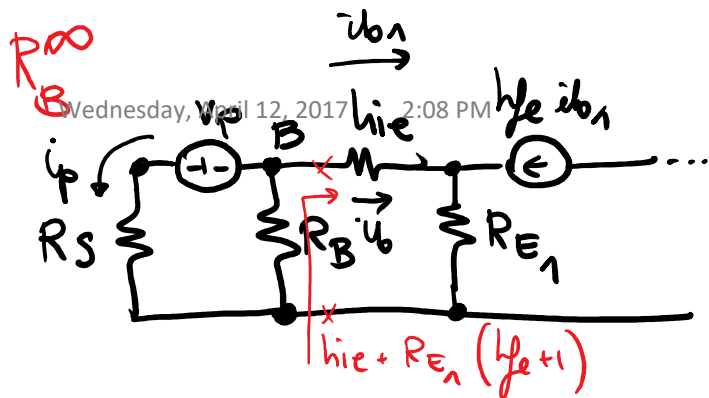


ciruito di piccolo segnale
IN BASSA FREQUENZA

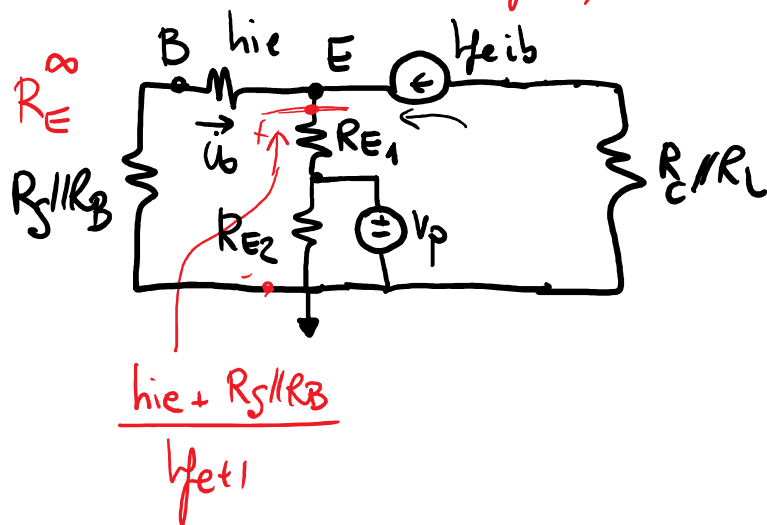


$$R_B = R_1 \parallel R_2$$

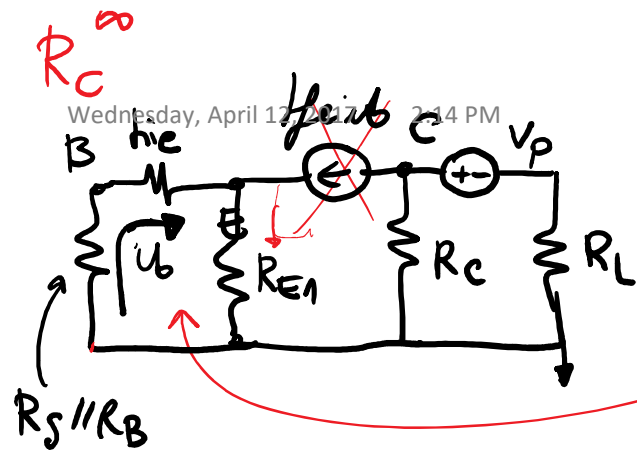
$$\omega_L = \frac{1}{R_B^{\infty} C_B} + \frac{1}{R_E^{\infty} C_E} + \frac{1}{R_C^{\infty} C_C}$$



$$R_B^{\infty} = [h_{ie} + R_{E1} (h_{fe} + 1)] \parallel R_B + R_S$$



$$R_E^{\infty} = \left\{ \left[\frac{h_{ie} + R_S \parallel R_B}{h_{fe} + 1} \right] + R_{E1} \right\} \parallel R_{E2}$$



$$[R_S \parallel R_B + h_{ie}] i_b + R_{E1} i_b (\beta + 1) = 0$$

$$\rightarrow i_b = 0$$

$$R_C^\infty = R_C + R_L$$